3-dimensional elastic beam model for large-deformation analysis of bending-active gridshells

Yusuke SAKAI (Kyoto University)

Makoto OHSAKI (Kyoto University)

Sigrid ADRIAENSSENS (Princeton University)

#### **Bending-Active Gridshell**



#### Dynamic Relaxation method for dynamically solving static problems <u>Scalar</u>



## Our goal:

# Proposing <u>3-dimensional elastic beam model</u> with <u>6 degrees of freedom</u>

 $\rightarrow$  Simple tool for form-finding of flexible beams



→ <u>No need</u> sophisticated software packages

# 3D elastic beam model using Unit normal vector



Describe the deformation of a beam element by using the unit normal vector at deformed state

#### Six variables at each end node of a beam element



**Translational displacements** 







#### Total potential energy

$$\Pi_{\text{total}} = \sum_{k=1}^{m} \prod_{int}^{k} - \sum_{j=1}^{s} \prod_{ext}^{j} EA \text{ Axial summess}$$

$$\Pi_{\text{total}} = \sum_{k=1}^{m} \prod_{int}^{k} - \sum_{j=1}^{s} \prod_{ext}^{j} EI_{i} \text{ Bending stiffness}$$

$$\Pi_{int}^{k} = \frac{EA}{2\overline{L}_{k}} e_{k}^{2} + \frac{GJ}{2\overline{L}_{k}} \left(\theta_{1(j+1)k} - \theta_{1jk}\right)^{2} \qquad EI_{i} \text{ Bending stiffness}$$

$$\Pi_{int}^{k} = \frac{EA}{2\overline{L}_{k}} e_{k}^{2} + \frac{GJ}{2\overline{L}_{k}} \left(\theta_{1(j+1)k} - \theta_{1jk}\right)^{2} \qquad U_{j} \text{ Translational disp.}$$

$$\frac{EA}{2\overline{L}_{k}} e_{k}^{2} + \frac{GJ}{2\overline{L}_{k}} \left(\theta_{2jk}\right)^{2} + 4\theta_{2jk}\theta_{2(j+1)k} + 4\left(\theta_{2(j+1)k}\right)^{2} \qquad H_{ijk} \text{ Rotational disp.}$$

$$\frac{EA}{2\overline{L}_{k}} e_{k}^{2} + \frac{GJ}{2\overline{L}_{k}} \left(\theta_{1(j+1)k} - \theta_{1jk}\right)^{2} \qquad H_{ijk} \text{ Rotational disp.}$$

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$$\frac{EA}{2\overline{L}_{k}} e_{k}^{2} + \frac{GJ}{2\overline{L}_{k}} \left(\theta_{2(j+1)k} + 4\left(\theta_{2(j+1)k}\right)^{2}\right)^{2} \qquad H_{ijk} \text{ Rotational disp.}$$

$$\frac{EA}{2\overline{L}_{k}} e_{k}^{2} + \frac{GJ}{2\overline{L}_{k}} \left(\theta_{2(j+1)k} + 4\left(\theta_{3(j+1)k}\right)^{2}\right)^{2} \qquad H_{ijk} \text{ Rotational disp.}$$

$$\frac{EA}{2\overline{L}_{k}} e_{k}^{2} + \frac{GJ}{2\overline{L}_{k}} \left(\theta_{2(j+1)k} + 4\left(\theta_{3(j+1)k}\right)^{2}\right)^{2} \qquad H_{ijk} \text{ Rotational disp.}$$

$$\frac{EA}{2\overline{L}_{k}} e_{k}^{2} + \frac{GJ}{2\overline{L}_{k}} \left(\theta_{2(j+1)k} + 4\left(\theta_{2(j+1)k}\right)^{2}\right)^{2} \qquad H_{ijk} e_{k}^{2} + \frac{GJ}{2\overline{L}_{k}} \left(\theta_{2(j+1)k} + \frac{GJ}{2\overline{L}_$$

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#### Example (material properties and methods)

$$E = 200$$
 GPa,  $D=0.03$  m,  $d=0.026$  m



Implement the proposed model

- 1. Dynamic Relaxation method (DRM)
- Optimization (OPT) → Minimize total potential energy (quasi Newton method)
- 3. Finite Element method (FEM)  $0.0 \le t_{\text{FEM}} \le 1.0$  Upward virtual load equal to self-weight  $1.0 \le t_{\text{FEM}} \le 2.0$  Forced disp. and External loads







#### Conclusions :

## 3-dimensional elastic beam model

Energy-based formulation + DRM algorithm
 No need tangent stiffness matrix

2. Unit normal vector at each end node >>No need large-rotation formulation

3. Proposed model + DRM algorithm >> can carry on large-deformation analysis of bending-active gridshells without sophisticated software packages